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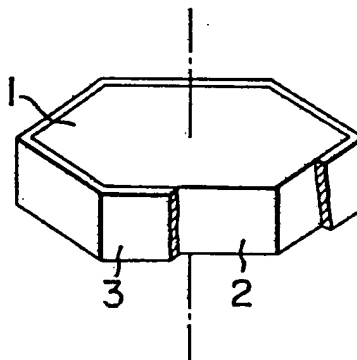
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54 Polygonal mirror and method of manufacturing the same.

57 A polygonal mirror and a method of manufacturing the same are disclosed in which a machined mirror surface (2) of an aluminum substrate or block (1) is anodized to form a transparent film (3) for protecting the mirror surface (2).



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POLYGONAL MIRROR AND METHOD  
OF MANUFACTURING THE SAME

1           The present invention relates to a polygonal  
mirror and a method of manufacturing polygonal mirrors,  
and more particularly to a polygonal mirror for laser  
beam scanning suitable for use in a laser printer and  
5 others.

A conventional optical reflecting mirror is  
formed in such a manner that a surface of a glass or  
metal substrate is lapped to a mirror surface finish,  
the surface thus lapped is coated with evaporated  
10 aluminum or the like through the vacuum evaporation or  
sputtering technique to increase the reflectivity of  
the surface, and the surface is further coated with a  
protection film. In recent years, however, an increase  
in the accuracy of a turning (or cutting) machine and  
15 an improvement in a cutting technique with a diamond  
cutting tool make it possible to form an optical mirror  
surface by a cutting operation.

A substrate of a conventional optical element  
having a mirror surface is made of glass or a hard  
20 metal capable of being lapped. The surface of the  
optical element is coated with evaporated aluminum in  
order to increase reflectance, and is further coated  
with a thin film of SiO or SiO<sub>2</sub> for mechanical protection.  
In such an optical element, the film of SiO or SiO<sub>2</sub>  
25 on the glass or hard metal substrate has a large

1 mechanical strength and can serve as a protection film  
even when the thickness of each of evaporated aluminum  
and the film of SiO or SiO<sub>2</sub> is small because the  
mechanical strength of such a thin film depends on the  
5 hardness of the substrate.

However, such a conventional optical element  
is high in cost and low in handling efficiency since  
the element is required to have a high reflection coating  
or film and a film for mechanical protection of the  
10 surface.

An object of the present invention is to  
provide a polygonal mirror in which highly reflective  
surface is formed by directly machining (or cutting) a  
surface of a substrate or a block made of aluminum or  
15 an aluminum alloy such as an Al-Mg alloy, an Al-Mg-Si  
alloy or an Al-Mn alloy.

Another object of the present invention is  
to provide a polygonal mirror which has a characteristic  
of high reflectance and is capable of producing a  
20 constant scanning light intensity in a range of scan  
angle.

Yet another object of the present invention  
is to provide a method for manufacturing such a polygonal  
mirror.

25 In order to attain these objects, a polygonal  
mirror according to the present invention is made of  
aluminum or an aluminum alloy, a reflecting surface of  
the mirror is cut to a mirror surface, and a protection

1 film is formed by anodizing the mirror surface.

The present invention will be apparent from the following detailed description taken in conjunction with the accompanying drawings, in which:

5 Fig. 1 is a perspective view showing a main part of a polygonal mirror according to the present invention;

Fig. 2 is a diagrammatic view for explaining interference of light caused by a single layer of thin  
10 transparent film;

Fig. 3 is a graph showing a relation between film thickness and reflectivity; and

Fig. 4 is a graph showing the variation of reflectivity with film thickness for a plurality of  
15 values of incident angle.

In order to realize a highly reflective polygonal mirror by fly-cutting, soft metal such as aluminum or aluminum alloys can be used and machined to a mirror surface. In the case of such an mirror  
20 mode of soft metal, however, a thin film formed on the surface of the mirror cannot act as a protection film having a high mechanical strength. Accordingly, it is required to form a thick  $\text{SiO}$  or  $\text{SiO}_2$  film on the  
surface. The  $\text{SiO}$  or  $\text{SiO}_2$  film is small in growth rate  
25 and therefore it is inefficient to form such a film. Further, an apparatus for forming the above film is expensive, and in addition to this, handling efficiency is low.

1           In order to solve such difficulties, a polygonal  
mirror according to the present invention is made of  
aluminum or an aluminum alloy, and the reflecting  
surface of the mirror is fly-cut to a mirror surface.  
5 Further, the mirror surface thus obtained is anodized  
to form a film for mechanical protection.

As mentioned above, according to the present  
invention, a surface of an aluminum substrate or block  
is directly cut to a mirror surface, and therefore the  
10 high-reflectivity characteristic of aluminum is utilized  
effectively. Thus, it is not required to form a high-  
reflectivity film, but only a protection film is  
required. Moreover, a thin transparent film acting as  
the protection film can be advantageously readily  
15 formed on the aluminum substrate or block by anodic  
oxidation. In other words, one of the advantages of  
the present invention resides in that the anodic  
oxidation is applied as an optical mirror surface  
processing to an aluminum substrate or block to which it  
20 has been hard to apply the optical mirror surface  
processing.

The use of anodic oxidation has the following  
advantages. That is, a thick film can be readily formed,  
and an anodic oxidation apparatus for forming such  
25 a film is simple in structure, as compared with an  
evaporation or sputtering apparatus. Further, the  
thickness of a film formed by anodic oxidation is  
proportional to the quantity of electricity having

1 flowed between electrodes, and therefore can be readily  
controlled. Thus, a protection film of good quality  
can be readily formed, and moreover the cost thereof  
can be reduced.

5 Now, a preferred embodiment of a polygonal  
mirror according to the present invention will be  
explained below, with reference to Fig. 1. In the  
figure, a block 1 of a polygonal mirror is made of  
aluminum or an aluminum alloy, the side surface of the  
10 block 1 is cut to mirror surfaces 2, and a thin trans-  
parent film 3 is formed by anodic oxidation to protect  
the mirror surfaces 2. The substrate 1 is preferably  
made of an Al-Mg alloy, which is suited for anodic  
oxidation. In the present invention, the film 3 formed  
15 by anodic oxidation does not lower the high reflectivity  
of the mirror surfaces, and moreover mechanically  
protects the surface of the block 1 made of a soft metal  
such as aluminum. The thin transparent film 3 produces  
a light interference phenomenon in accordance with the  
20 thickness thereof, that is, the reflectivity of the  
film 3 varies with the film thickness. Further, in the  
case where the polygonal mirror is rotated to carry out  
optical scanning, the incident angle of light at each  
mirror surface 2 varies with the rotational angle of  
25 the polygonal mirror, and thus the film thickness in  
the optical sense in the protection film 3 varies with  
the above-mentioned rotational angle. A change in the  
optical film thickness in the protection film 3 causes

1 a change in the interference condition, and therefore  
the intensity of scanning light varies with the rota-  
tion of the mirror. The above-mentioned facts will be  
explained with reference to Fig. 2. In the figure,  
5 the thin transparent film 3 having a refractive index  
 $n_1$  is formed, by anodic oxidation, on a mirror  
surface 2 of the aluminum block 1 having a refractive  
index  $n_0$ . Now, let us consider the case when a medium  
outside the film 3 has a refractive index  $n_2$  equal to 1.  
10 Then, the intensity  $R$  of reflected light is given by  
the following equation:

$$R = \frac{r_1^2 + r_0^2 + 2r_1r_0 \cos \delta}{1 + r_1^2 r_0^2 + 2r_1r_0 \cos \delta}$$

where  $r_1$  indicates the amplitude of light reflected  
from the upper surface of the film,  $r_0$  the amplitude of  
15 light reflected from the lower surface of the film,  $\delta$  an  
angle equal to  $4\pi n_1 d \cos \theta_r / \lambda$ ,  $\theta_r$  an angle of refrac-  
tion,  $d$  the thickness of the film 3 formed by anodic  
oxidation, and  $\lambda$  the wavelength of light.

When the factors  $n_0$ ,  $n_1$ ,  $n_2$ ,  $\theta_r$  and  $\lambda$  are  
20 kept constant, the intensity  $R$  of reflected light is a  
function of the thickness  $d$  of the film 3 and a  
periodic function with respect to optical film thickness  
 $n_1 d$ . In the case of normal incidence, the intensity  $R$   
of reflected light varies periodically with the optical  
25 thickness  $n_1 d$  of the film 3, as shown in Fig. 3.

In the present embodiment, the refractive

1 indices  $n_0$ ,  $n_1$  and  $n_2$  have a relation  $n_0 > n_1 > n_2$ , and  
 therefore the film 3 can act as an antireflection film.  
 As is apparent from Fig. 3, in order to make maximum  
 the intensity of reflected light, it is necessary to  
 5 make the optical film thickness  $n_1 d$  equal to  $m\lambda/2$ . In  
 a polygonal mirror for optical scanning, however, the  
 optical film thickness  $n_1 d$  for making maximum the  
 intensity of reflected light is not constant, since the  
 incident angle  $\theta$  of light at the upper surface of the  
 10 film 3 varies with the rotation of the polygonal mirror.

Now, let us consider the case where the  
 incident angle  $\theta$  varies from  $\theta_1$  to  $\theta_2$  to obtain an  
 optical scanning range. Then, the film thickness  $d$  for  
 making maximum the intensity of reflected light varies  
 15 from  $d_{\theta_1}$  to  $d_{\theta_2}$ , and the values  $d_{\theta_1}$  and  $d_{\theta_2}$  are given  
 by the following equations:

$$d_{\theta_1} = \frac{m\lambda}{2n_1 \cos \theta_{r1}}, \quad d_{\theta_2} = \frac{m\lambda}{2n_1 \cos \theta_{r2}}$$

where  $\sin \theta_1 = n_1 \sin \theta_{r1}$ ,  $\sin \theta_2 = n_1 \sin \theta_{r2}$ ,  
 $d_{\theta_1} < d_{\theta_2}$ , and  $m$  is a positive integer other than zero.

20 Fig. 4 shows the variation of the intensity  
 of reflected light with the optical film thickness for  
 some values of incident angle. Referring to Fig. 4,  
 when a reflecting mirror is rotated so that the incident  
 angle is changed from  $\theta_1$  to  $\theta_2$ , the optical film thick-  
 25 ness for making maximum the intensity of reflected light  
 varies with the above rotation. In more detail, for



1 the incident angle  $\theta_1$ , the intensity of reflected light  
varies with the optical film thickness as indicated  
by a curve 6. On the other hand, for the incident angle  
 $\theta_2$ , the intensity of reflected light varies as indicated  
5 by a curve 8. Accordingly, in the case where a reflect-  
ing mirror having the film thickness capable of making  
maximum the intensity of reflected light when light  
impinges upon the mirror at the incident angle  $\theta_1$ , is  
rotated so that the incident angle is changed from  $\theta_1$   
10 to  $\theta_2$ , the intensity of reflected light varies from a  
point A to a point B. On the other hand, in the case  
where a reflecting mirror having the film thickness  
capable of making maximum the intensity of reflected  
light when light impinges upon the mirror at the incident  
15 angle  $\theta_2$  is rotated, the intensity of reflected light  
varies from a point D to a point C.

For an incident angle  $\theta_0$  corresponding to the  
the center of the optical scanning range, the intensity  
of reflected light varies with the optical film thick-  
20 ness as indicated by a curve 7. When the thickness of  
the film takes a value  $d_{\theta_0}$  in order for the intensity  
of reflected light to be maximum at the incident angle  
 $\theta_0$ , the variation of the intensity of reflected light  
with the incident angle can be made smallest as shown  
25 in Fig. 4, that is, the intensity of reflected light  
varies only in a range from a point E to a point F.  
Accordingly, the optical thickness of the film is set  
so that the intensity of reflected light is maximum at

- 1 the incident angle  $\theta_0$  corresponding to a central portion  
of the optical scanning range, that is, is made equal  
to  $n_1 d \theta_0 (= m\lambda/2 \cos \theta_{r_0})$ .

As has been explained in the foregoing

- 5 description, according to the present invention, a  
protection film is high in transparency, and therefore  
the thickness of the film can be made large to increase  
the mechanical strength thereof, thereby producing a  
remarkable protection effect. Further, since the film  
10 is formed by anodic oxidation, the growth rate of the  
film is high. Furthermore, the film can be formed  
without using expensive apparatuses such as an evapora-  
tion apparatus and a sputtering apparatus, and therefore  
a polygonal mirror according to the present invention  
15 is advantageous from the economical point of view.

C L A I M S:

1. A polygonal mirror comprising:  
a block (1) having a surface (2) machined with precision to mirror, said block being made of aluminum or an aluminum alloy; and  
a transparent film (3) formed by anodizing said surface (2) machined with precision to mirror and used as a protection film for said mirror surface (2).
2. A polygonal mirror according to Claim 1, wherein said transparent film (3) has a thickness of  $m\lambda/2n_1 \cos \theta_{r_0}$ , where  $\theta_{r_0}$  indicates an angle of refraction of incident light corresponding to a central portion of an optical scanning range,  $n_1$  a refractive index of said transparent film (3),  $\lambda$  a wavelength of light and  $m$  a positive integer other than zero.
3. A polygonal mirror according to Claim 1, wherein said aluminum alloy further contains at least Mg.
4. A method for manufacturing a polygonal mirror comprising the steps of preparing a block (1) of aluminum or an aluminum alloy, cutting said block to provide a mirror surface (2) thereon, anodizing said block for forming a transparent film on said mirror surface to thereby protect said mirror surface.

FIG. 1

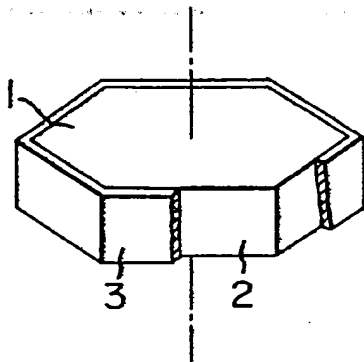


FIG. 2

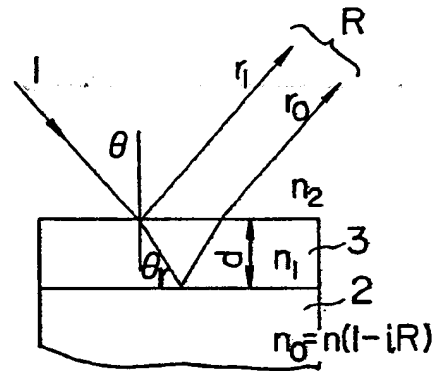


FIG. 3

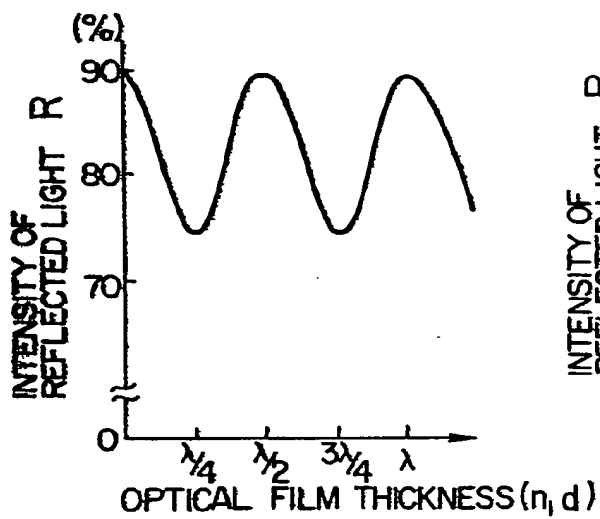
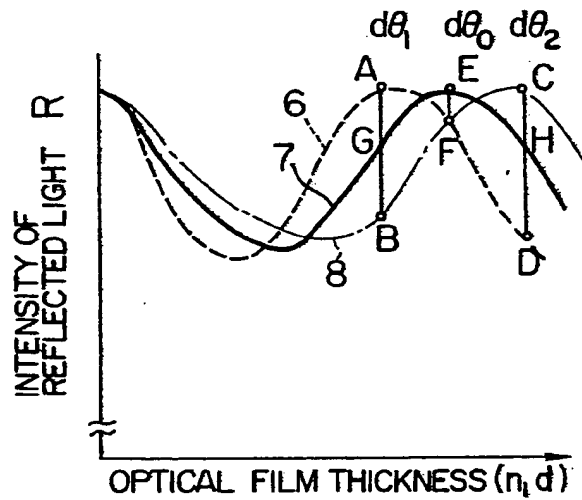


FIG. 4





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# EUROPEAN SEARCH REPORT

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EP 83 10 3960

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 7)
Y	FEINWERKTECHNIK & MESSTECHNIK, vol. 88, no. 7, 1980 M. KUPKA et al. "Diamantfräsen hochgenauer Metallspiegel", pages 346-350, chapter 2.9	1,4	G 02 B 5/18
Y	--- APPLIED OPTICS, vol. 18, no. 23, 1979 F. COOKE "Generation of a spherical mirror in aluminum", pages 3878, 3879	1,4	
Y	--- APPLIED OPTICS, vol. 17, no. 14, 1978 J. T. COX et al. "Protected Al mirrors with high reflectance in the 8-12-micron region from normal to high angles of incidence", pages 2125, 2126	1	
A	--- DE-C- 110 178 (C. ZEISS) * Claim 1 * -----	1,3	TECHNICAL FIELDS SEARCHED (Int. Cl. 7) G 02 B 5/08
The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 25-07-1983	Examiner FUCHS R
<b>CATEGORY OF CITED DOCUMENTS</b>			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	

